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Title: Insights into fractures and minerals in subbituminous and

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Abstract: Fractures are the main pathways for fluid transport, which constrain the coalbed methane (CBM) reservoir permeability. Permeability is one of the key petrophysical parameters for CBM production. The fractures in the low and middle rank coals usually filled with minerals, which can significantly reduce the reservoir permeability. In this study, X-ray μ -CT combined with field emission scanning electron microscopy (FESEM) together with energy dispersive spectrometry (EDS) were used to quantitatively evaluate the features of fractures and minerals of FK sample (Ro, max 0.65%) and ML sample (Ro, max 1.49%) including morphology, complexity, volume and 3D structure, and its impacts on permeability. The results showed that fractures are well developed as observed in the samples FK and ML by the 2D cross section of X-ray μ -CT. Dolomite and kaolinite are common in the samples FK and ML as confirmed by FESEM images with EDS. Moreover, the 3D fracture structure including the open fracture and mineral filled fracture were reconstructed. The quantitative structural parameters (e.g. length, width, area and volume) of the fractures for these two samples were acquired by the commercial software Avizo 9.0.1. The middle rank coal of sample ML has larger fracture density (181 fractures per mm3) than that of the low rank coal of sample FK (104 fractures per mm3). Based on the reconstructured 2D and 3D fracture structure, the fracture complexity was evaluated through fractal dimension. And the impacts of mineralization in coals on petrophysical properties were evaluated, which show that the connectivity of fractures, porosity and permeability were greatly improved after demineralization. Therefore, this study may have implications for enhancing CBM recovery through demineralization.

Highlights (for review)

Highlights

- Fractures and minerals of two Chinese coals were reconstructed by X-ray μ -CT.
- The open and mineralized fractures were quantitatively analyzed.
- Discrepancy of fractures and minerals in medium and low rank coals was evaluated.
- The importance of demineralization to enhance CBM production was illustrated.

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Insights into fractures and minerals in subbituminous and

2 bituminous coals by FESEM-EDS and X-ray μ-CT

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Abstract: Fractures are the main pathways for fluid transport, which constrain the coalbed methane (CBM) reservoir permeability. Permeability is one of the key petrophysical parameters for CBM production. The fractures in the low and middle rank coals usually filled with minerals, which can significantly reduce the reservoir permeability. In this study, X-ray μ -CT combined with field emission scanning electron microscopy (FESEM) together with energy dispersive spectrometry (EDS) were used to quantitatively evaluate the features of fractures and minerals of FK sample ($R_{o,max}$ 0.65%) and ML sample ($R_{o,max}$ 1.49%) including morphology, complexity, volume and 3D structure, and its impacts on permeability. The results showed that fractures are well developed as observed in the samples FK and ML by the 2D cross section of X-ray μ -CT. Dolomite and kaolinite are common in the samples FK and ML as confirmed by FESEM images with EDS. Moreover, the 3D fracture structure including the open fracture and mineral filled fracture were reconstructed. The quantitative structural parameters (e.g. length, width, area and volume) of the fractures for these two

samples were acquired by the commercial software Avizo 9.0.1. The middle rank coal of sample ML has larger fracture density (181 fractures per mm³) than that of the low rank coal of sample FK (104 fractures per mm³). Based on the reconstructed 2D and 3D fracture structure, the fracture complexity was evaluated through fractal dimension. And the impacts of mineralization in coals on petrophysical properties were evaluated, which show that the connectivity of fractures, porosity and permeability were greatly improved after demineralization. Therefore, this study may have implications for enhanced CBM recovery through demineralization.

Keywords: fractures; minerals; CT; FESEM-EDS; demineralization

1. Introduction

Coalbed methane (CBM) is a form of unconventional natural gas extracted from coal reservoirs. In the past few decades, CBM has become a substantial source of clean energy, of which the exploration and development have been successfully carried out in many countries such as US, Australia, and Canada [1]. China has rich coal resources and abundant CBM resources. The CBM exploration and development in China has been developing rapidly in recent years. Statistically, the CBM resources below the depth of 2000 meters reach $36.81 \times 10^{12} \, \text{m}^3$ and over $16000 \, \text{CBM}$ wells including vertical and horizontal wells were drilled in China with an annual CBM output of $70.2 \times 10^8 \, \text{m}^3$ [2].

During the process of CBM production, gas flows through the fractures to the wellbore in response to the pressure gradient [3]. When the reservoir pressure drops below the critical CH₄ desorption pressure, the adsorbed CH₄ gradually diffuses from the micropores in coal

matrix to the macropores or fractures [4, 5] Therefore, the fractures are the main pathways for gas and water flow. Normally the in-situ fractures were filling with minerals, which have significant impacts on the fracture properties, and thus on fracture permeability. For instances, minerals that include inherent or extraneous minerals (e.g. quartz, clay minerals, feldspars, carbonates, and sulphide minerals) are often developed in the coal fractures [2]. The inherent or extraneous minerals present differently in coals. Inherent minerals are normally syngenetic, which are generally enclosed by or embraced in coal matrix, while extraneous mineral are filling in fractures [3]. Therefore, the extraneous minerals can substantially reduce the reservoir permeability and affects the process of gas production [4, 5]. The fracture morphology, connectivity and density can be system acquired with multiple techniques (e.g. optical microscope, AFM, FESEM, CT and NMRI) [5-7]. CT as a non-destructive technique has been widely used to investigate the 3D structure of coals, which can obtain the specific fracture parameters including fracture length and surface area [8]. Although the X-ray μ-CT can distinguish the fractures, minerals and coal matrix, the specific minerals (e.g. quartz and feldspars,) cannot be detected [9, 10]. In this study, an X-ray μ-CT combined with field emission scanning electron microscopy and energy dispersive spectrometry will be adopted to acquire the 3D structure information of fractures and minerals in coals. Fracture complexity and irregularity can be described with the fractal geometry [11-14]. Fractal dimension (D) is an important characteristic parameter of fractal geometry, which can quantitatively reflect the fracture complex in coals. Therefore, the fractal dimension may indicate the CBM adsorption and flow capabilities [15]. The fractal dimension of fractures in coals can be acquired by scanning electron microscopy (SEM), nuclear magnetic resonance

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67 (NMR), mercury intrusion porosimetry and low-temperature N2 adsorption/desorption 68 isotherm [16-18]. The X-ray μ -CT scanning can capture the detailed fracture structure in both 69 2D slices and 3D reconstruction patterns. 70 In this study, X-ray μ-CT together with FESEM-EDS scanning will be used to accurately 71 characterize the multiscale characteristics of 2D and 3D fracture structure and minerals 72 performance in the low rank coal sample FK and medium rank coal sample ML. Herein, the 73 fractal dimension of fractures in 2D and 3D view will be calculated, and the original and 74 de-mineralized coals will be compared to evaluate the effects of mineralization on fracture 75 properties. Firstly, the morphology of fractures and minerals were identified in 2D 76 FESEM-EDS. Secondly, X-ray μ-CT scanning was combined to accurately characterize the 77 multiscale characteristics of 3D fractures and minerals. And the fracture complexity and 78 irregularity were described with the fractal geometry. Finally, the impacts of fractures and 79 minerals performance on petrophysical properties including porosity and permeability were 80 detail discussed. This study provided a possible way to enhance CBM recovery through 81 demineralization.

2. Experiments and methods

83 2.1. Coal basic information

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One subbituminous coal from Fukang (FK) colliery in the southern Junngar Basin and another bituminous coal from Malan (ML) colliery in the northwest Qinshui Basin were collected, which were drilled for cylindrical cores with 25mm in diameter and 50mm in length approximately. With Leitz MPV-3 photometer microscope, maceral composition analysis and the maximum vitrinite reflectance ($R_{o, max}$) were performed on polished slabs as previous

research [7]. The proximate analysis was conducted on the Automatic Proximate Analyzer

5E-6600. The results as listed in Table 1 indicated that FK sample was a subbituminous coal

with R_{0, max} of 0.65% that belong to low rank coal and the ML sample was a bituminous coal

92 with $R_{o, max}$ of 1.49% that belong to medium rank coal.

2.2. X-ray μ-CT scanning and FESEM-EDS

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The CT measurements of the FK and ML samples were performed on the nanoVoxel-3502E microfocus X-ray CT scan equipment. The cylindrical core samples (9.77mm in diameter and 15mm in length for sample FK, and 5.64mm in diameter and 10mm in length for sample ML) was placed perpendicular to the sample couch, and was aligned in the center of the scanner field of view. The X-ray source voltage and current were set to be 120KV, 36.67µA and 70KV, 40µA for the FK and ML samples, respectively. The CT equipment is able to produce a voxel dataset containing a series of 2D slices with the resolution of 500 nm. The detector has a resolution of 2048×2048 pixels, in which each pixel represents an area of ~3.98×3.98um² for sample FK and 2×2um² for sample ML respectively. The spatial resolution of sample FK and ML are approximately 3.98 µm and 2 µm, with which most fractures can be distinguished. Field emission scanning electron microscope (FESEM) with an energy dispersive spectrometer and X-ray diffractometer were used to aid microfocus X-ray CT method and recognize the mineral matter [19]. Coal samples were polished into lumps approximately 10 mm (length) ×10 mm (width) × 7 mm (height) with spluttered thin gold coating. The fractures and mineral band in the range of 3nm-50µm can be measured using the FEI Quanta FEG 450 (FEI, America) and EDAX TEAM EDS.

111 2.3. 3D morphology reconstruction

For a typical CT grayscale image, each pixel corresponds to a grayscale that equals to specific CT number. Normally, minerals with high CT number (approximately 3000 HU) present white, whereas the fractures with low CT number (<600HU) show black, and coal matrix with medium CT number (100-1600HU) correspond to a certain range of gray [8]. Then 3D threshold segmentation (watershed segmentation), the process of partitioning of the greyscale image into unique phases, was applied according to CT number. After that the partitions were colored and the 3D model of each partition was established. The image data from the X-ray μ -CT was imported into Avizo 9.0.1, the commercial software for 3D visualization, reconstruction and analysis. The representative elemental volume (REV) under the subvolume extraction is important due to the computational capability of the computers and the coal strong heterogeneity [20]. The size of digital core REVs for sample FK and ML was determined to be 2000 μ m × 2000 μ m × 2000 μ m to assess the properties of organics, fractures and minerals with thousand 2D slices stacked together.

125 2.4. Fractal dimension calculation of fractures

The fractals of fractures can be evaluated by box-counting dimension method, fractal Brown motion method and area measurement method [21]. In this study, 2D and 3D box-counting methods were employed to calculate the fractal dimension of 2D slices and reconstructed REV. The box-counting method divides the image space or volume into square boxes of each size δ . By decreasing the size of the square boxes by half, the number of square boxes $N(\delta)$ contained fractures can be counted, which depends on the size of the square box [22]:

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$$N(\delta) \sim \delta^{-D}$$
 (1)

- Then, a log-log plot composed of the number of the boxes $N(\delta)$ versus the different size of
- boxes δ can be plotted. Finally, the linear fitting equation can be established below:

$$\log(N(\delta)) = -D\log(\delta) + \log(\alpha) \tag{2}$$

- Where, $N(\delta)$ is the number of square boxes contained fractures, δ is the size of square
- boxes, α is constant, and D is the fractal dimension of fractures.
- 138 2.5. Permeability evaluation
- 139 The absolute permeability simulation can be conducted through Avizo XLab Extension with a
- 140 finite volume method. The equations used in the absolute permeability simulation are
- discretized on a staggered grid to allow a better estimation of the no-slip boundary condition.
- 142 Before absolute permeability simulation, the isolated fracture space should be removed and
- extract the connected fracture space through Avizo software. The aim is to assure that the
- 144 fracture space existing in the samples allows fluid pass through. The definition of absolute
- permeability is based on Darcy's law:

$$\frac{Q}{S} = -\frac{k}{\mu} \frac{\Delta P}{L} \tag{3}$$

- Where Q is the flow rate (m³ per second); S is the cross section area (m²); k is the absolute
- permeability (m²); μ is the dynamic viscosity of the fluid (Pa·s); Δ P is the pressure difference
- (Pa); L is the sample length in the flow direction (m).
- 150 To numerically estimate absolute permeability, the Stokes equations are solved:

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$$\begin{cases} \overrightarrow{\nabla} \cdot \overrightarrow{\nabla} = 0 \\ \mu \nabla^2 \xrightarrow{V} - \xrightarrow{\nabla} P = \xrightarrow{0} \end{cases}$$
 (4)

- Where $\frac{1}{\nabla}$ is the divergence operator; $\frac{1}{\nabla}$ is the gradient operator; $\frac{1}{\nabla}$ is the velocity of the
- 153 fluid in the fluid phase of the material; μ is the dynamic viscosity of the flowing fluid; ∇^2 is
- the Laplacian operator; P is the pressure of the fluid in the fluid phase of the material. This

simplified Navier-Stokes equations considering an incompressible fluid means the density is a constant; A Newtonian fluid means the dynamic viscosity is a constant; A steady-state flow means the velocity does not vary over time; A laminar flow means the concerned velocities are small enough not to produce turbulence. The simulated flow direction can be adjusted to X, Y or Z direction respectively. The inflow pressure was set to be 1.3×10^5 Pa, the outflow pressure was set to be the atmospheric pressure, and the water viscosity is 1.005×10^{-3} Pa·s.

3. Results and discussion

3.1. 2D morphology of fractures

Fig. 1 shows the typical 2D morphology of fractures obtained by X-ray μ-CT, which can be divided into two categories: syngenetic fractures (also named cleats) that formed during the process of coalification, and exogenous fractures that formed during deformation and faulting by tectonic movements [23]. The cleats commonly occur in orthogonal fractures, face cleats and butt cleats (a1-2, b1-2 in Fig. 1) [24]. Face cleats formed first during coalification, and butt cleats formed later and terminated by face cleats [25]. Face cleats were dominant and extensive, which were wider than butt cleats [26]. The face cleats were basically filled with minerals, whereas no mineralization was observed in butt cleat (a1-2, b1-2 in Fig. 1). Cleat-filling minerals were epigenetic, which mainly precipitate along the face cleats from the solutions with various compositions and temperatures [27].

With the aid of energy dispersive spectrometer, the main fracture filling minerals of sample FK and ML are identified as dolomite (a3 and a4 in Fig. 1) and kaolinite (b3 and b4 in Fig. 1), which indicates that the minerals were deposited by the movement of mineralized fluid through the coal seam after the development of major fractures. Gypsum are widely spread in

the coal matrix as inherent minerals in the sample FK, and calcite and pyrite occurs as individual grains in coal matrix of the sample ML. Mineral in threshold segmentation can be divided into two categories: fracture-filling minerals and scattered minerals in both sample FK and ML. FESEM imaging (a3 and b3 in Fig. 1) shows the width of open fractures in sample FK and ML are in the range of 0.59-1.83μm and 1.335-12.6μm, while mineralized fractures are in the range of 6.07-40.56μm and 0.13-66.85μm respectively. The width of mineral-filling fracture varies greatly compared with the open fractures and mineralized fluids mainly flow in large fractures with the width greater than 10μm.

185 3.2. 3D reconstructed fractures

3D fracture reconstructed structures were established by 2D X-ray μ-CT slices to determine the fracture networks. A1 and b1 in Fig. 2 shows that the 3D reconstructed volumes of original FK and ML coals were divided into coal matrix in black, fractures in blue and minerals in yellow. A2 and b2 Fig. 2 shows the 3D structure of FK and ML coals after grayscale threshold segmentation. Fractures are composed of unmineralized fractures in blue, mineral filled fractures in pink. And scattered minerals within coal matrix are presented in yellow. Herein, the mineral filled fractures are the same as fracture filled minerals due to the same threshold segmentation. The volume fraction of each part was calculated through the number of pixels (volume) by CT scanning. The volume fractions of scattered minerals for the samples FK and ML are 0.55% and 13.98% respectively. The mineral-filled fractures or fracture-filling minerals accounts for 10.77% and 7.46% for the samples FK and ML respectively, which occupy 96.42% and 90.31% of the total fractures. Therefore, most fractures in both sample FK and ML were filled with minerals and these fractures that filling

minerals may inhibit the fluid flow process due to the decrease in fracture width of the seepage path, which is unfavorable for CBM production, especially when the mineral filled fractures have wonderful connectivity (a2 and b2 in Fig. 2). Therefore, demineralization could be an effective way to increase the fluid flow path and the fractures connectivity, and thus possibly increase the permeability.

- 3.3. The evaluation of fractures complexity
- 205 3.3.1. Structure evaluation of fractures

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The fracture density for sample FK was 839 fractures within the volume of 8 mm³ (149 open fractures and 690 mineral-filling fractures per mm³), whereas 1451 fractures per 8 mm³ (1436 open fractures and 15 mineral-filling fractures per mm³) for sample ML, which indicates that more fractures developed in sample ML than that of sample FK. During coalification (R_o _{max}<0.65%), the dehydration and volatiles loss will result in the formation of microfractures [28]. When R_{o, max}>1.30%, the fracture density will decrease slowly and then remain constant with increasing coal rank [29]. The structural parameters (average length, average width, average area and average volume) for open fractures, mineral-filling fractures and total fractures of the two samples were presented in Table 2 and Fig. 3. 3D visualization of open fracture and total fracture in different length scale were presented in Fig. 4. The average width and average volume in sample ML are reduced by 45.94% and 56.78% compared to sample FK and the other average structural parameters including fracture length, area decrease with increasing coal rank (low-rank to medium-rank). At the early coalification of R_o. _{max}=0.6%-1.2%, overburden pressure results in structural parameters decreased with the increase of coal rank [30-32]. When R_{o,max} is in 1.25%-2.25%, the small-molecule compounds

continue to decrease because of the overburden pressure and matrix shrinkage, but the rate of decline slows [33]. Mineral-filling fractures occupy 96.42% and 90.31% volume in total fractures for samples FK and ML, which means most fractures are filled with minerals carried by underground fluid. The average width of total fractures increased by 4.46% and 9.87% compared to open fractures and the maximum fracture width changes from 35.95µm to 55.81µm and 19.11µm to 98.96µm for samples FK and ML respectively, which indicates that the fluid flow space will be greatly improved if mineral-filling fractures are de-mineralized. 3.3.2. Fractures complexity by fractal dimension Fractal method was used to evaluate the complexity of fractures [25]. Generally, the microfractures become much more complex as coal rank increase, which leads to the high fractal dimension [31]. The 2D and 3D fractal dimension of open and total fracture of FK sample were calculated by box dimension method as shown in Fig. 5. The following size of square or cube is used (in pixels): 4, 8, 16, 32 and 64. The calculation for obtaining 2D and 3D fractal dimension can be seen in Fig. 6. For 2D fractal dimension of fractures, 16 slices were selected evenly to calculate the 2D fractal dimension for sample FK and ML respectively. 2D fractal dimension of fractures varies from slice to slice due to the strong heterogeneity. However, the 3D fractal dimension can represent the fracture complexity of the whole sample. The average 2D and 3D fractal dimensions of open fractures in sample ML are 1.16 and 2.172 respectively, which are lower than those of sample FK (1.25, 2.242). Whereas the average value of total fractures for sample ML are 1.50 and 2.519, which are higher than

escape from the coal as gases (H₂O, CO₂, and CH₄) and the average structural parameters

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those of sample FK (1.44, 2.403) after demineralization. Therefore, the fractal dimension of

fractures in de-mineralized samples, whether 2D or 3D fractal dimensions, increased greatly compared with original open fractures, which means that the value of fractal dimension increases with the degree of fracture development. The 2D and 3D fractal dimension of original open fractures in sample ML are lower than those of sample FK. However, both 2D and 3D fractal dimension of total fractures in sample ML exceed those in sample FK after demineralization for mineral-filling fractures. Therefore, the mineralization of sample ML is more serious.

- 250 3.4. Insights into petrophysical properties of coals
- 251 3.4.1 Fracture porosity

The fracture porosity of the original open and de-mineralized fractures was numerically calculated to evaluate the effect of minerals on permeability. The fracture porosity of samples FK and ML were obtained from micro-CT data as shown in Fig. 7. For original open fractures, the open fracture porosity in different directions has an average difference of 2.1%, while the total fracture porosity included de-mineralized fractures shows variable porosity with an average difference of 6.3% in different directions, which indicate that the fracture has strong heterogeneity in different directions. The fracture porosity varies from slice to slice. For sample FK and ML, the average total fracture porosity of the de-mineralized samples are 6.85% and 11.47%, which increased by 6.39% and 10.37% compared with original open fractures porosity. If the minerals-filling fractures are de-mineralized or acidified, these fractures will be favorable for enhancing CBM recovery. Fig. 8 shows the correlation between the fractal dimensions of fractures and CT fracture porosity. The CT porosity shows an approximately U-shaped change with 2D fractal dimensions or 3D fractal dimensions, which

presents similar tendency: porosity firstly decreases from 1.1% to 0.46%, then increases with fractal dimension increasing.

3.4.2. Fracture permeability

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The fracture connectivity is another important factor influencing permeability in coals. Fig. 9 show the 3D spatial distribution of connected/unconnected fractures of original samples (a1 and b1 in Fig. 9) and de-mineralized samples (a2 and b2 in Fig. 9), respectively. The volume fractions of connected fractures in open and total fractures for sample FK are 33% and 89%, respectively. For sample ML, the volume fractions of the connected fracture are 54.1% and 98.4% in open and total fractures, respectively, which indicated that more than half of the open fractures are isolated. And most mineral-filling fractures are well connected with other, which will result in the favorable fluid flow path in fractures after mineral removed. The connective fractures, as effective flow paths, can cause permeability increase for water/gases. In this work, the absolute permeability simulation was conducted based on visualized geometrical properties by micro-CT images [30]. The absolute permeability sharply increase from 400 mD to 450 mD for sample FK and 0 mD to 740 mD for sample ML in the Y axis after demineralization, and increase by 92% and 25% in Z axis after mineral removed, which indicates that more connected fractures were provided for fluid flow. Therefore, de-mineralization or acidification could be very important way for enhancing CBM production. One thing that needs to clear is the result from numerical simulation varied widely from laboratory result, which attribute to the significant interactions of gas, water and fracture-wall that can significantly influence the permeability [31]. Pores that have been neglected in the simulation also occur in coal, which also can make contribution to coal permeability [34]. The difference of permeability indicates the importance of de-mineralization of mineral filling fractures. Therefore, this fracture permeability simulation with and without mineral filling can be conducive to enhancing CBM production.

4. Conclusions

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X-ray μ-CT and field emission scanning electron microscope (FESEM) together with energy spectrum experiment (EDS) can be used as effective means to evaluate fracture structure and mineral performance in different rank coals (samples FK and ML). The structure, fracture porosity, connectivity and permeability of open fracture and total fractures was quantitatively evaluated by 2D and 3D fracture model and calculated to illustrate the effect of minerals on flow capability. The following conclusions are made: 1) The well developed microfractures and dolomite and kaolinite filled microfractures present in samples FK and ML, which were confirmed by FESEM images and 2D slices of X-ray μ-CT together with EDS. The 3D reconstructed open fractures and total fractures of samples FK and ML show the significantly changes in fracture structure. 2) The variable structure parameters (e.g. length, width) indicate that coal rank has significant influence on fracture structure. The fracture density in medium rank coal (sample ML) is two times than that in low rank coal (sample FK), while the structural parameters (average fracture length, width, and volume) reduce as coal rank increase. The fracture structure becomes more complex with the growth of fractal dimensions due to the matrix shrinkage and overburden pressure during the coalification jump. 3) The permeability simulation reveals that the structural parameters (e.g. fracture porosity, connectivity and permeability) of the fractures and the minerals have important impacts on permeability. The volume of connected fractures and the porosity sharply increased after mineral removal, which can significantly improve the permeability. Therefore, demineralization or acidification can be used to increase the void space and connectivity of the mineral-filling fractures, and will be favorable for enhancing CBM production.

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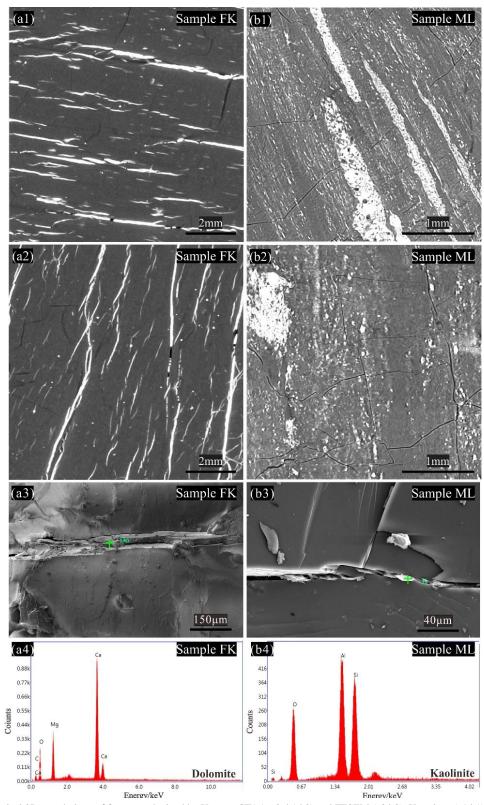


Fig.1 Typical 2D morphology of fractures obtained by X-ray μ -CT(a1, a2, b1,b2) and FESEM (a3,b3). X-y plane (a1,b1) and y-z plane (a2,b2) cross-section of sample FK and ML. Fractures in sample FK filled with dolomite (a3) and the spectrum obtained from a point on dolomite's surface (a4). Fractures in sample ML filled with kaolinite (b3) and the spectrum obtained from a point on dolomite's surface (b4).

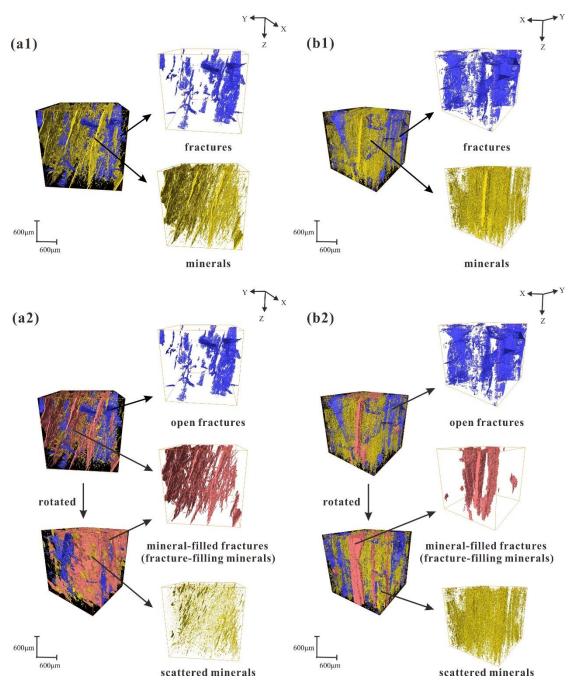


Fig.2 3D visualization of original sample FK (a1) and ML (b1), re-segmented sample FK (a2) and sample ML (b2). For original samples (a1,b1), coal matrix are shown in black, fractures are shown in blue and minerals components are shown in yellow. For re-segmented samples (a2, b2), open fractures are shown in blue, mineral-filled fractures (fracture-filling minerals) are shown in pink, and scattered minerals are shown in yellow.

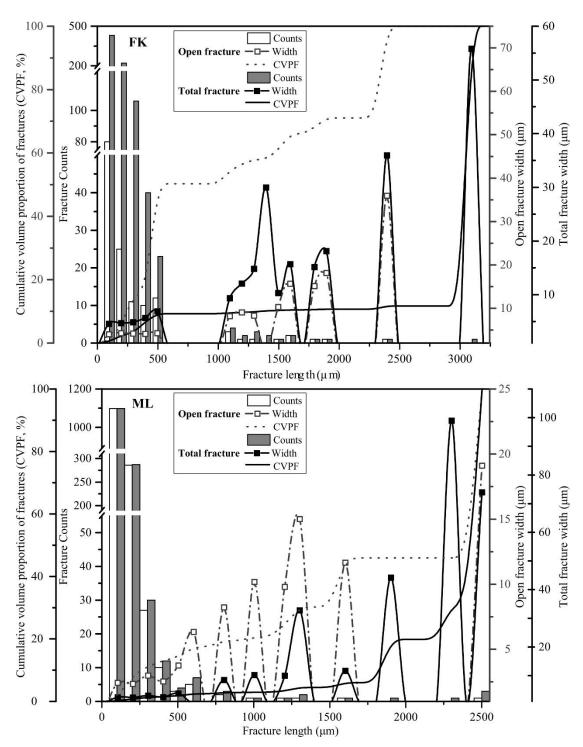


Fig.3 The counts, average width and cumulative volume proportion of open fracture and total fracture in different length scale.

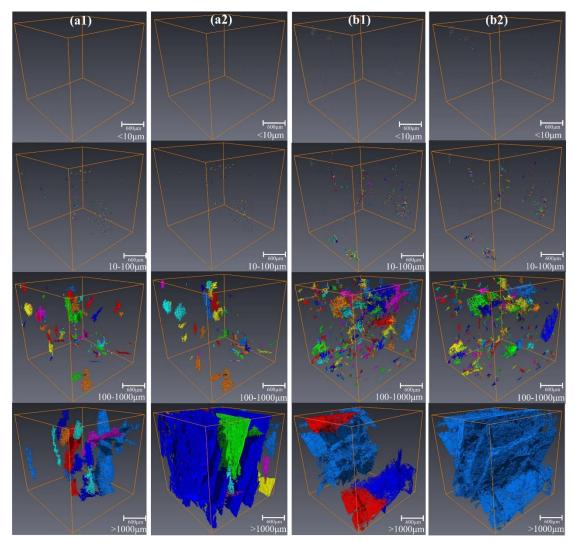


Fig.4 Different length scale of open fractures and total fractures in sample FK and ML: Fractures length<10 μ m, 10-100 μ m, 100-1000 μ m and >1000 μ m. (a1) Open fractures in sample FK; (a2) Total fractures in sample FK. (b1) Open fractures in sample ML. (b2) Total fractures in sample ML.

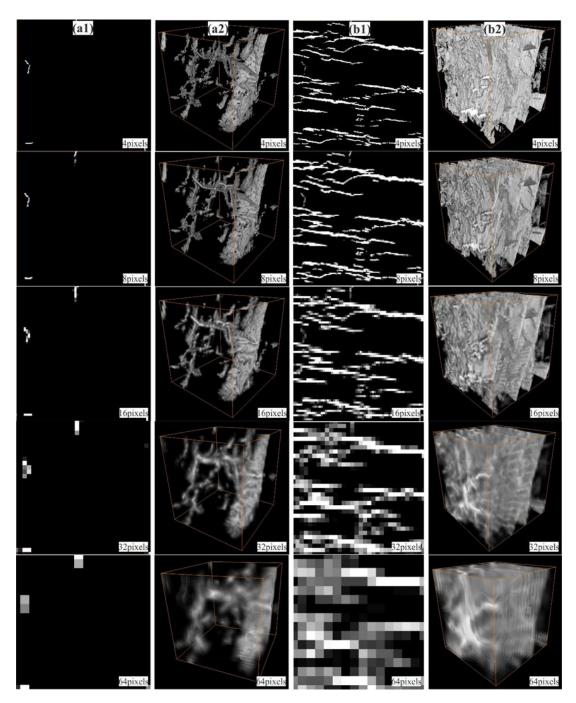


Fig.5 Two dimension (2D) and three dimension (3D) fractal dimension calculation prosses of fracture in sample FK. (a1) 2D fractal dimension calculation prosses of open fracture, taking the 1st section along Z axis as example; (a2) 3D fractal dimension calculation prosses of open fracture in sample FK; (b1) 2D fractal dimension calculation prosses of total fracture, taking the 1st section along Z axis as example; (b2) 3D fractal dimension calculation prosses of total fracture in sample FK. The size of square or cube were used (in pixels):4,8,16,32,and 64,espectively.

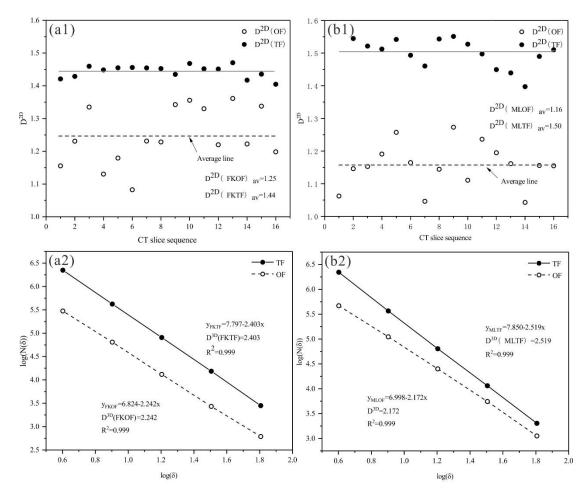


Fig.6 The results of two dimension(2D) and three dimension(3D) fractal dimension of samples FK and ML. (a1)The 2D fractal dimension of open and total fractures in sample FK along Z axis direction; (a2)The 3D dimension of open and total fractures in sample FK; (b1) The 2D fractal dimension of open and total fractures in sample ML along Z axis direction; (b2) The 3D dimension of open and total fractures in sample ML. Notes: OF: Open fracture; TF: Total fracture.

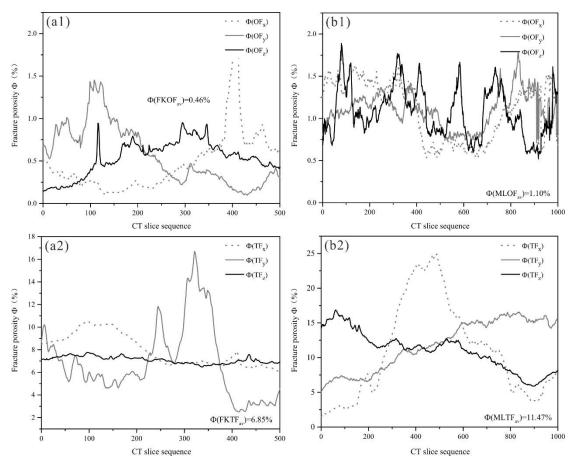


Fig.7 Fracture porosity of original (Φ (OF)) and de-mineralized (Φ (TF)) of samples FK and ML in different directions. (a1) Fracture porosity of original sample FK (Φ (FKOF)); (a2) Fracture porosity of de-mineralized sample FK (Φ (FKTF)); (b1) Fracture porosity of original sample ML (Φ (MLOF)); (b2) Fracture porosity of de-mineralized sample ML (Φ (MLOF)). Notes: OF: Open fracture; TF: Total fracture.

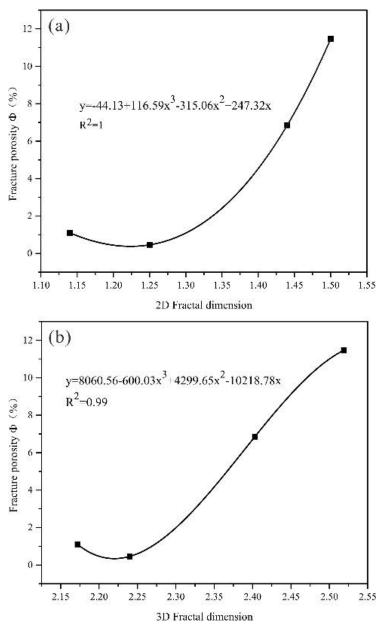


Fig.8 The correlation between the fractal dimensions ((a):2D fractal dimension; (b)3D fractal dimension). Porosity firstly decreases and then increases with fractal dimension increasing, displaying a 'U-shaped' trend.

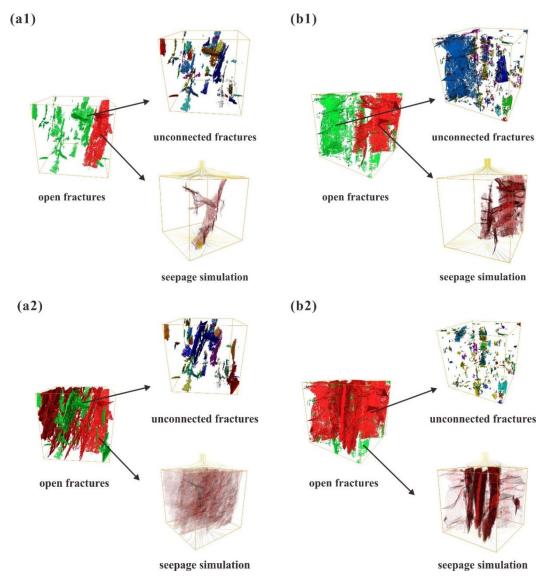


Fig.9 Results of connectivity analysis showing 3-D distribution of connected-unconnected fractures in original and de-mineralized sample FK (a1 and a2) and sample ML (b1 and b2). Further seepage simulation of connected fractures and 3-D distribution analysis of unconnected fractures were carried out. Connected fractures are shown in red and unconnected fractures are shown in green.

Table 1 Petrographic and proximate analysis results for two Chinese coals

Sample	$R_{o,max}$	Coal rank	Coal composition (Vol. %)			Proximate analysis (wt. %)			
No.	(%)		Vitrinite	Inertinite	Exinite	Mad	Aad	Vad	FCad
FK	0.65	subbituminous coal	83.9	1.7	14.5	3.76	8.86	39.21	48.17
ML	1.49	bituminous coal	67.6	32.4	0	0.29	9.97	14.73	75.01

 $R_{o, m}$ = maximum vitrinite reflectance under oil immersion; Mad = moisture content (wt. %, air dry basis); Aad = ash yield (wt. %, air dry basis); Vad = volatile matter (wt. %, air dry basis); FCad = fixed carbon (wt. %, air dry basis).

Table 2 The average structural parameters of open fractures and mineral-filled fractures in sample FK and ML.

Comple	Structural	al Fracture type			
Sample		Open fractures	Mineral-filled	Total fractures	
no.	parameter		fractures		
	AL (µm)	67.55	81.56	76.80	
FK	$AW\ (\mu m)$	4.83	5.10	5.05	
FK	$AA\ (\mu m^2)$	5.23×10 ⁴	1.00×10^{5}	8.91×10^{4}	
	$AV\ (\mu m^3)$	2.16×10^{5}	1.33×10^{6}	1.07×10^{6}	
	$AL\ (\mu m)$	58.82	934.30	67.87	
M	$AW\ (\mu m)$	2.48	26.21	2.73	
ML	$AA\ (\mu m^2)$	2.20×10^4	5.57×10^6	7.93×10^4	
	$AV\ (\mu m^3)$	4.46×10 ⁴	4.03×10 ⁷	4.61×10 ⁵	

Notes: AL=average length; AW=average width; AA=average area; AV=average volume.

Table 3 Comparison of structural parameters between open fractures and total fractures, sample FK and ML.

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Relative growth rate	Sample no.		Relative decline rate	Fracture type		
between OAT (%)	FK	ML	between FAM (%)	Open fracture	Total fracture	
AL	15.84	15.39	AL	12.92	13.27	
AW	4.46	9.87	AW	48.74	45.94	
AA	67.69	261.39	AA	58.71	11.01	
AV	390.07	933.39	AV	79.51	56.78	

Notes: AL=average length; AW=average width; AA=average area; AV=average volume; OAT=open fractures and total fractures; FAM=FK and ML sample.