The use of high resolution graphite furnace molecular absorption spectrometry (HR - MAS) for total fluorine determination in extractable organofluorines (EOF)

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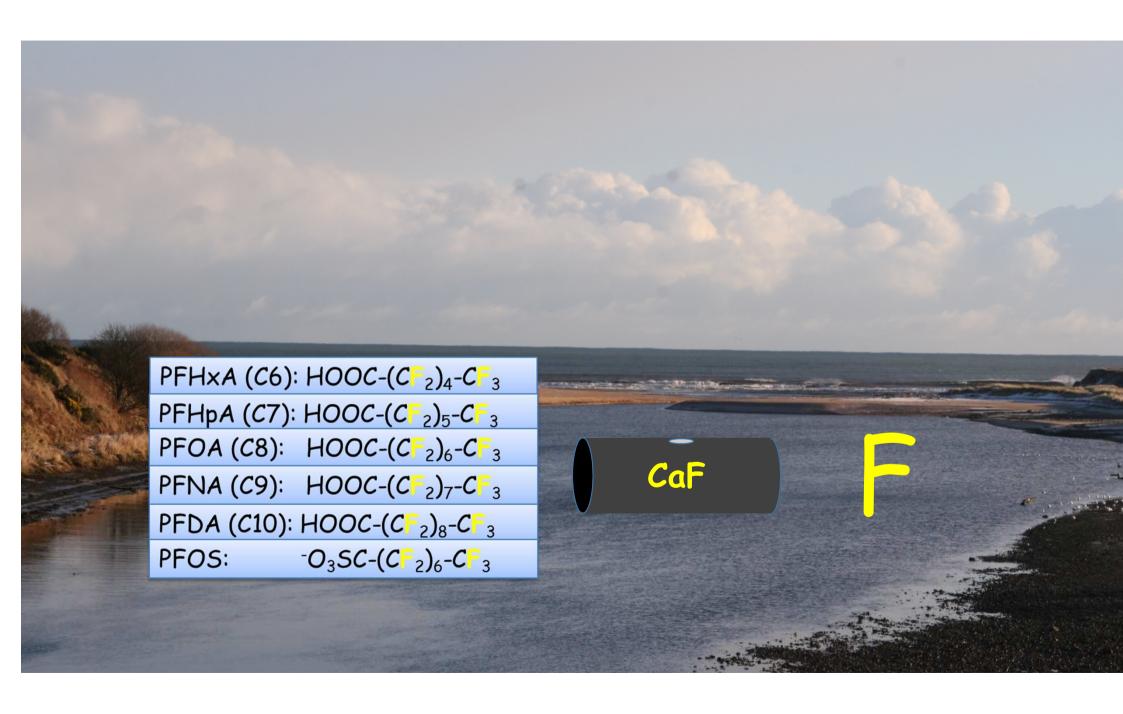
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1	THE USE OF HIGH RESOLUTION GRAPHITE FURNACE MOLECULAR
2	ABSORPTION SPECTROMETRY (HR -MAS) FOR TOTAL FLUORINE
3	DETERMINATION IN EXTRACTABLE ORGANOFLUORINES (EOF)
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## 23 Abstract:

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The determination of total fluorine content using high-resolution graphite furnace continuum source molecular absorption spectrometry (HR- MAS) has been employed in a variety of samples for over 10 years. However, most of the samples analysed by HR- MAS are rich in fluoride, with negligible levels of organic fluorinated species. With an increase in concern surrounding per- and polyfluoroalkyl substances (PFASs), new methods to measure total fluorine of organofluorine using different techniques have been developed. However, no studies focused on PFASs behaviour in HR-MAS have been performed. As these compounds encompass a wide range of different structures, boiling points, decomposition temperatures and matrix interactions, a loss of accuracy can occur when an aqueous external calibration is performed using only one compound. To overcome this issue, an investigation into permanent modifiers for the graphite furnace was performed. After optimisation similar sensitivity for different PFCA was achieved when 400 µg of W was used as a permanent modifier together with an optimised temperature program. The relative deviation between the different PFCA standard slopes relative to the PFOA slope was lower than 15%. The instrumental limit of detection and quantification (LOD and LOQ, respectively) of total fluorine as total PFCA was 0.1 mg L<sup>-1</sup> and 0.3 mg L<sup>-1</sup>, respectively, while the method LOD and LOQ (using solid phase extraction) was 0.3 µg L<sup>-1</sup> and 1.0 µg L<sup>-1</sup>, respectively. The developed method gave satisfactory recoveries for the spiked PFCA into seawater, river water and effluent using PFOA calibration standards. The optimised method is useful for measuring extractable organofluorines (EOF) when only ionic PFASs such as PFCA are expected. When other organofluorines are expected, the results using HR GF-MAS should be taken with caution.

- 48 KEYWORDS: per- and polyfluoroalkyl substances, HR-MAS, fluorine
- 49 determination, POP, PFAS.

## 1. Introduction

Fluorine is essential for human health. Enhance fluorine analysis in water and food is mandatory. However, most common methods are actually determine only the amount of fluoride such as ion selective electrode (ISE) or ion chromatography [1]. This is because only fluoride is known to protect from dental decay and promotes healthy bones, due to its role in proper calcium mineralization and formation of dental enamel [2]. The European Food Safety Authority (EFSA) recommends an intake of 0.05 mg of fluoride per kg of body weight per day for children and adults [3], and the World Health Organization (WHO) recommends fluoride concentrations between 0.8 and 1.5 mg/L in drinking water [4]. Alongside this, humans are exposed to fluoride through breathing air and foods such as dill, cucumber and pickles [5]. However, an excess of fluoride in the diet may cause dental or skeletal fluorosis which can lead to staining and even high porosity in dental enamel, ligaments calcification and bone lesions, with accumulative effects [6].

Besides the concern caused by excessive uptake of fluoride, humans may be exposed to fluorine via organofluorine compounds, which are used extensively as pharmaceuticals, anaesthetics, agrochemicals, refrigerants and industrial polymers [7]. Of particular concern are per- and polyfluoroalkyl substances (PFASs) which are a class of over 4000 anthropogenic chemicals containing one or more fully fluorinated carbon atoms. PFASs are widely used in consumer products, including cosmetics, food packaging, and textiles [8]. PFASs tend to be highly persistent and accumulate in human blood globally. As opposed to most persistent organic pollutants, which have been studied for a long time with well-known side-effects from their indiscriminate use, investigations into the effects of PFASs are still in their infancy [10]. The reason for such lack of concern about this class of compounds is

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in the stability of C-F bound, with an average bond energy 485kJ/mol [11,12], which causes many scientists to believe in a supposed lower reactivity of organofluorine compounds [9]. Believed to be inert and safe, these compounds were produced on an industrial scale before being considered an emerging pollutant due their nondegradable and bioaccumulative properties, leading them to recently become a hot topic [13]. The chronic and acute toxicities of various PFASs have been analysed due to the potential threat they pose to humans and wildlife. These analyses showed **PFASs** demonstrate carcinogenicity. hepatotoxicity. that immunotoxicity. developmental toxicity and affect hormones [14]. There have also been studies that show the residence time for PFASs in humans to be longer than that in laboratory animals [15], leading to even greater concern over their effect on human health and the need for regulation of PFASs in consumer products.

In 2009, perfluorooctane sulfonate (PFOS) and related PFASs were added to Annex B of the United Nations Stockholm Convention on Persistent Organic Pollutants, in order to reduce and eventually eliminate the use of PFASs in industry, recognising PFASs as a threat to human health and the environment [16]. This recognition of the need for regulation is important yet requires appropriate methods of analysis to monitor. However, the measurement of PFASs is much more challenging than other chlorinated and brominated compounds [17] due to the huge number of structurally different chemicals. Despite the different behaviour routinely only dozen of PFASs are monitored using HPLC-ESI-MS/MS in targeted analysis [18]. Hence, fractionation schemes have been developed which would determine the amount of total fluorine, extractable organofluorines (EOF) [19,20] to determine the extent of PFASs and other organofluorines through a mass balance approach [21].

99 For total fluorine a few methods have been described in the literature such as PIGE, 100 INAA and CIC and recently compared for food packeting material [22].

On the other hand, spectroscopic techniques exhibit great potential for application to total fluorine determination, the current methods include laser-induced breakdown spectroscopy, and inductively coupled plasma mass spectrometry [23–26].

Here in this study we focussed on the use of high-resolution molecular absorption spectrometry (HR-MAS) for the determination of total fluorine. HR-MAS involves the formation of a metal monofluoride such as GaF, and CaF, and the measurement of its molecular absorption bands within the range of commercially available AAS. This technique has been used for fluorine determination due its robustness, low operational cost when compared to the plasma techniques, high analytical throughput, presenting accurated results with simple or even any sample preparation procedure, once optimized temperature program and permanent modifier is able to remove interferences efficiently.

Dittrich et al. [27] investigated using HR-MAS with a graphite furnace (GF) for the determination of halogens using different forming reagents such as Ga, Al, Tl, In and Mg salts. Morés et al. [28] investigated the most sensitive wavelength for CaF and found this to be 606.440 nm for the determination of total-F in tea which is most likely only fluoride with small amounts of fluoroacetate. Other successful studies have used CaF to measure the total-F content in milk and coal [29,30]. For these cases, when Ca was used as the forming reagent, neither permanent (which can be impregnated onto the platform surface after a temperature program) nor chemical modifiers in solution (added in the graphite tube with the sample) were not used.

All papers mentioned above describe an analysis of total fluorine content of different samples, however no studies investigating different fluorinated compounds behaviour in HR-GF MAS were performed. Since an expressive part of the fluorine is in the inorganic form, any loss of accuracy caused by a difference in sensitivity between the inorganic standard used for calibration and the organofluorine species present in the sample would be negligible. However, if an organic extraction is performed, the quantification of the extractable organofluorine using external calibration with inorganic standards can lead to inaccurate results, since the behaviour of organofluorine in a graphite furnace remains unknown. Different boiling points, decomposition temperatures and interactions with the permanent modifier can occur, resulting in differences in sensitivity of the organofluorine compounds.

This study presents an investigation into the thermal behaviour of the most common PFASs, with the development of a method able to quantify the sum of all organofluorines occurring in the different classes of PFASs present in a methanolic solution, as a tool for fluorine mass balance. The study was executed through the application of different permanent modifiers, in order to reduce the deviation in sensitivity among different PFASs. The accuracy of the developed method was assessed by standard addition followed by solid phase extraction (SPE) in different water samples (sea water, river water, effluent and wastewater).

#### 2. Experimental

#### 2.1 Instrumentation

A high-resolution continuum source atomic absorption spectrometer (model contrAA 700, Analytik Jena, Jena, Germany) was used for all measurements. The spectrometer was equipped with a xenon short-arc lamp with a nominal power of 300 W operating in a hot-spot mode, which emits a spectral continuum between 190 and

900 nm and a charge-coupled device (CCD) array detector with 588 pixels, 200 of which are used for analytical purposes. The double monochromator consists of a prism pre-monochromator and an echelle grating monochromator for high resolution. All measurements were performed using the wavelength of highest sensitivity for CaF at 606.429 nm, using the sum of the integrated absorbance of three pixels (peak volume selected absorbance, PVSA, A $\Sigma$ 3,int) [31]. Pyrolytically coated graphite tubes with PIN platform (Analytik Jena, Germany) and with transversal heating were used in all experiments.

## 2.2 Materials and reagents

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Ultrapure water with a resistivity of 18.2 M $\Omega$  cm (Smart2 Pure, Thermo Fisher Scientific, Loughborough, UK) was used for the preparation of the standard solutions. The fluorine standard was prepared from 1 g L<sup>-1</sup> F from KF in water (Thermo Fisher Scientific) and Ca(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O (VWR chemicals, Leicestershire, UK) was used as a forming-reagent at a concentration of 1% Ca (w/v). 1H,1H,2H,2Hperfluorohexanol (4:2 FTOH), 1H,1H,2H,2H-perfluorodecanol (8:2 FTOH) and 1H,1H,2H,2H-perfluorododecanol (10:2 FTOH) were obtained from Flurochem Ltd (Hadfield, UK) while perfluorooctanoic acid (PFOA), perfluorodecanoic acid (PFDA), perfluorohexanoic acid (PFHxA). perfluoroheptanoic acid (PFHpA). perfluorohexanesulfonic acid (PFHxS) and potassium PFOS were obtained from Sigma Aldrich (St Louis Mo, USA). PFAS solutions were prepared in methanol (MeOH, Merck, Darmstadt, Germany) and then diluted with ultrapure water. 99.998% purity argon gas was provided by BOC (Dublin, Ireland). For sample preparation, 98% formic acid was used (Fisher Scientific, Loughborough, UK), methyl tert-butyl ether (MTBE) (Merck), ammonium hydroxide (Merck), For coating the graphite furnace Pd, Pt, W (Merck) and Zr (VWR, Leicestershire, England) standard solutions

were used. Mg (NO<sub>3</sub>)<sub>2</sub> (Merck) was used mixed with Pd(NO<sub>3</sub>)<sub>2</sub> as a chemical modifier in solution.

## 175 2.3 Samples

All optimisations were performed with 1:1 MeOH/ H<sub>2</sub>O standard of PFOA, PFOS, PFHxS, FTOH 10:2, FTOH 8:2 and FTOH 4:2 at a concentration of 5 mg F L<sup>-1</sup>.

The developed method was applied to river water (River Don, Aberdeen, Scotland), sea water (Aberdeen Bay), wastewater and effluent samples (from Nigg WWTW in Aberdeen, Scotland). The sample preparation for the aqueous standards for the calibration curve and the samples, except waste water was performed according to Zacs et al. [32]. Around 200 mL of the centrifuged sample (3000 rpm for 5 minutes) where weighed and spiked with 0, 1 and 2 ng fluorine each as PFOA, PFOS, PFHxS, PFHpA, PFDA and PFHxA respectively and 100 µL formic acid.

For the wastewater samples, around 10 g (w/w) of sample was spiked with 0, 1 and 2 ng fluorine each as PFOA, PFOS, PFHxS, PFHpA, PFDA and PFHxA and left to equilibrate for at least 30 minutes. 5 mL of MeOH and 1 mL of 0.2 mol L<sup>-1</sup> NaOH were then added. The samples were vortex-mixed and submitted to a 30 minutes ultrasound bath before subsequent centrifugation at 3000 rpm for 10 minutes. The supernatant was then transferred to a 50 mL PP falcon flask and 50  $\mu$ L of formic acid was added.

The samples were added to Oasis weak anion exchange cartridges (Waters Technologies, US), previously conditioned with 3 mL of 30% NH<sub>4</sub>OH, 3 mL of MTBE/MeOH (90:10 v/v), 3 mL of MeOH and 3 mL of deionized water. After loading the samples, the cartridges were washed with 1 mL of 2% formic acid and 2 mL of

MeOH. After drying for 30 minutes under vacuum, the cartridges were eluted with 7 mL of MTBE. The eluates were dried under a stream of nitrogen at 40  $^{\circ}$ C and reconstituted with 200  $\mu$ L of MeOH. In order to fit in the working range, the samples were diluted 100 times just before the quantification. The analysis were carried out in a W-coated graphite furnace platform and submitted to the temperature program according to the Table 1.

**Table 1.** Temperature program for F determination via CaF in a W-coated graphite furnace platform. Gas flow MAX in all steps except vaporization step.

Step	Temperature / °C	Ramp / °C s <sup>-1</sup>	Hold / S
Dry 1	70	6	15
Dry 2	70	0	5
Pyrolysis	700	300	10
Vaporization	1900	3000	5
Clean	2100	1000	5

## 2.4 Graphite furnace platform coating

For atomic absorption spectrometry, the permanent modifiers are classified in two groups: platinum group modifier (PGM) and carbide former modifier (CFM), presenting different mechanisms of action with the analyte. Since the thermal behaviour of the diatomic molecules and the interaction with permanent modifiers at high temperatures remains unknown, four permanent modifiers, two from PGM (Pd and Pt) and two from CFM (Zr and W) and a mixture of Pd/Mg nitrates as chemical modifier in solution were chosen for this study. 400 µg of Pd, Pt, Zr or W were used for the permanent graphite platform recoating and a temperature program

optimisation was performed by the multivariated study of drying temperature and the univariated study of pyrolysis and vaporization temperature. For platform recoating, ten injections of 40  $\mu$ L of a 1 g L<sup>-1</sup> solution of each permanent modifier were used. After each injection, the temperature program described in Table 2 was performed.

Table 2. Temperature program for Pd, Pt, W or Zr coating. Gas flow MAX in all steps.

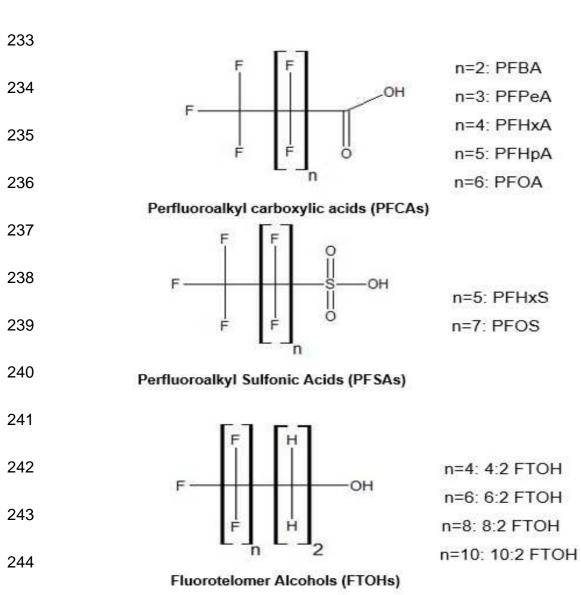
Step	T / °C	Ramp / °C s <sup>-1</sup>	Hold / s
1	90	5	40
2	110	1	40
3	130	1	40
4	1200	300	25
5	2100	500	10
6	2100	0	5

## 3. Results and Discussion

## 3.1 Per- and polyfluoroalkyl substances

In order to characterise the different behaviour of different common classes of PFASs containing ionic and neutral compound with different volatility and water solubility (Table 2), six different PFASs were chosen: PFOA, PFOS, PFHxS, and 3 FTOHs (10:2, 8:2 and 4:2; Figure 1).





**Figure 1.** Chemical structures of a selection of per- and polyfluoroalkyl substances.

These compounds are distinguished by different functional groups. While PFCA are carboxylic acid and negatively charged in natural waters, PFOS and PFHxS are also negatively charged sulphonic acids. FTOHs are alcohols with different numbers of fluorine-substituted carbons and neutral. Alongside the different physicochemical features such as volatility and solubility, these structural and

functional differences could cause different interactions with the graphite surface and modifiers, resulting in different sensitivities and a loss of accuracy, since the inorganic fluoride calibration standard might not behave in the same way as the mixture of PFASs present in the matrix. Since it is not possible to optimise a method for all the known PFASs, these analytes were chosen to be investigated as representatives of compounds with their respective functional groups.

**Table 3.** Physicochemical properties of the studied PFASs.

Compound	Molar weight	Solubility in water	Melting point	Boiling point
	(g/mol)	at 25 °C (g/L)	(°C)	(°C)
4:2 FTOH	264.09	0.97 <sup>b</sup> [33]	-58 [34]	140-143 [34]
8:2 FTOH	464.12	0.194x10 <sup>-3</sup> [35]	46-50 [33]	112-114 [35]
10:2 FTOH	564.13	8,9 x 10 <sup>-4 b</sup> [36]	90-95 [37]	110-145 [37]
PFOA [38]	414.1	9.5	40 - 50	189 -192
PFOS <sup>a</sup> [38]	538 <sup>a</sup>	0.68 <sup>a</sup>	>400 <sup>a</sup>	NDA
PFHxS	400.11	6.2 x10 <sup>-3</sup> [39]	NDA	238-239 [40]

a: K salt. b: at 22 °C NDA: No data available.

## 3.2 Temperature program

As showed in the Table 3, the volatility of the FTOHs is significantly higher than the other PFASs. This can cause loss of the analyte during drying and pyrolysis in the graphite tube. To overcome this issue, a Doehlert multivariate experimental design was performed for each drying step and the temperature and hold time for 4:2, 8:2 and 10:2 FTOH were optimised. For this experiment, 5  $\mu$ L of a 5 mg F L<sup>-1</sup> solution of each FTOH and 5  $\mu$ L of a 1% (w/v) Ca aqueous solution were used. The experimental matrix is shown in Table 4.

Table 4. Doehlert experimental design matrix for optimisation of drying step forFTOHs.

Experiment	Drying 1 hold time (s)	Drying 1 temperature (°C)
1	7	70
2	13	70
3	15	80
4	13	90
5	7	90
6	5	80
7 (c)	10	80
7 (c)	10	80
7 (c)	10	80
Experiment	Drying 2 Hold time (s)	Drying 2 temperature (°C)
Experiment 1	Drying 2 Hold time (s) 7	Drying 2 temperature (°C) 70
1	7	70
1 2	7	70 70
1 2 3	7 13 15	70 70 80
1 2 3 4	7 13 15 13	70 70 80 90
1 2 3 4 5	7 13 15 13 7	70 70 80 90
1 2 3 4 5 6	7 13 15 13 7 5	70 70 80 90 90 80
1 2 3 4 5 6 7(c)	7 13 15 13 7 5	70 70 80 90 90 80

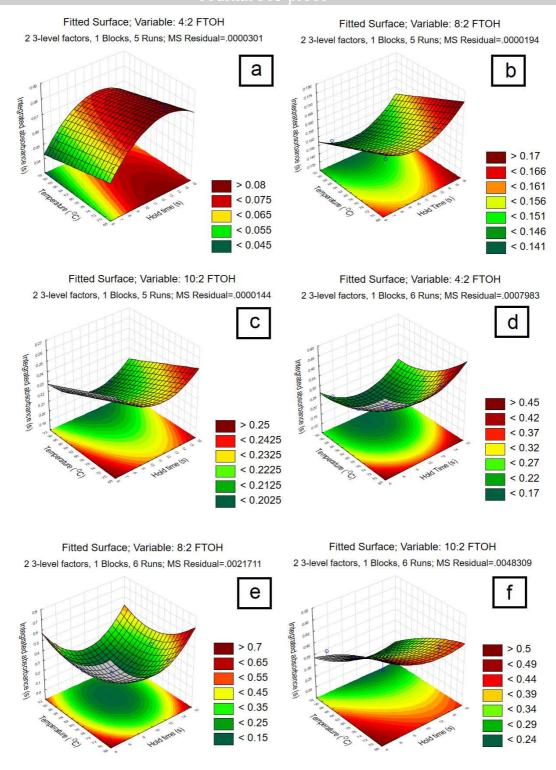
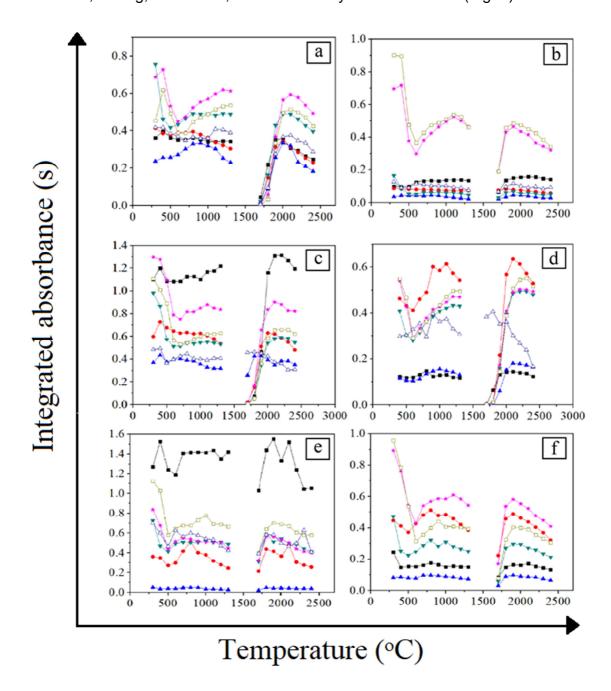


Figure 2. Response surface for a Doehlert experimental design. For the drying 1 step: a) 4:2 FTOH b) 8:2 FTOH c) 10:2 FTOH. For the drying 2 step: d) 4:2 FTOH e) 8:2 FTOH f) 10:2 FTOH. All experiments were performed with a total of 25 ng of F,  $T_{pyr}$ : 900 °C,  $T_{vap}$ : 2000 °C in a W-coated graphite tube.

According to the results shown in Figure 2a, for the drying 1 step, the temperature had less influence on the most volatile compound 4:2 FTOH (flat curve and low sensitivity), and was more critical for 8:2 and 10:2 FTOH, which shows a significant increase in instrumental response at lower temperatures (Fig. 2b and c). The fact that this parameter was not significant for 4:2 FTOH may be interpreted as a non-ideal range of study for this compound due to its high volatility, but lower temperatures were not able to satisfactorily dry the solvent. In this study, a longer hold time in a lower temperature produced a more intense signal, with an efficient dry without boiling, which causes loss of analyte by spilt in the windows/wall of the graphite furnace. Also, the lower temperatures avoid losses by volatilization. The same was observed for all analytes and for this reason, the drying 1 temperature was fixed at 70 °C and held for 15 seconds.

About the Drying 2 step, the different temperatures and hold times did not show any improvement for 4:2 FTOH (Fig. 2d), again, probably caused by a non-ideal range of study. For 8:2 FTOH and 10:2 FTOH (Fig. 2e and f), the losses were avoided with a low temperature with a short hold time. By the visual observation of the sample during the drying 2 step, it was possible to ensure the short hold time was enough for a completely dry. For this step, the optimal conditions were fixed at 70°C and 5 seconds.

The pyrolysis and vaporization steps were univariately optimised for all the studied compounds. 5 µL of a 5 mg F L<sup>-1</sup> solution from each compound and 5 µL of a 1% (m/v) Ca aqueous solution were used in this experiment. The thermal behaviours of F<sup>-</sup>, PFOA, PFOS, PFHxS, 10:2 FTOH, 8:2 FTOH and 4:2 FTOH were investigated



**Figure 3.** Optimisation of temperature program for aqueous standards of (■) fluoride; (△)10:2 FTOH; (●) 8:2 FTOH; (▲) 4:2 FTOH; (▼) PFOA; (□) PFHxS and (★) PFOS performed with 25 ng of F and a) 400 μg of Zr as permanent modifier; b) 400 μg of Pd as permanent modifier + 7.5 ng/ 5 μg of the mixture of Pd/Mg nitrates in

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solution; c) 400  $\mu$ g of W as permanent modifier; d) without any permanent modifier; e) 400  $\mu$ g of Pt as permanent modifier and f) 400  $\mu$ g of Pd as permanent modifier. For all pyrolysis optimisations  $T_{vap}$ : 2000 °C and for vaporization optimisations  $T_{pyr}$ : 900 °C.

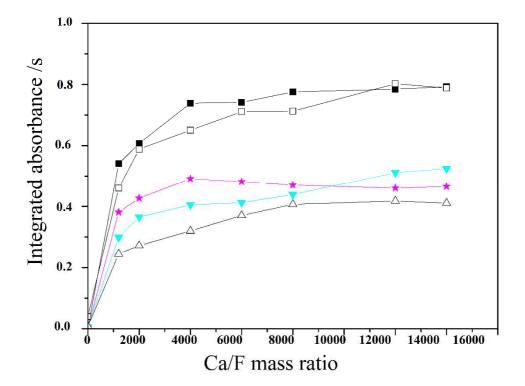
The main concern regarding determination of total fluorine in an extract is the variation in sensitivity among individual PFASs especially if the fluorine speciation in the extract is unknown. This can lead to inaccurate results as the calibration with fluoride may not be representative of all compounds. As observed in Figure 3, the studied compounds showed not only different thermal behaviours, but their behaviours also varied when different modifiers were used. For the tube without a permanent modifier (Fig. 3d), 4:2 FTOH and fluoride gave the same intensity, but around five times lower than the other analytes. For the Zr-coated graphite tube (Fig. 3a), all tested PFASs and fluoride had a similar intensity when a pyrolysis temperature of 700 °C and vaporization temperature of 1900 °C were used. This indicates that the permanent modifier Zr is necessary to stabilize fluorine especially from the volatile species. When Pd/Mg was used as a chemical modifier in solution (Fig 3b), most of the substances presented similar and low sensitivity (excepting PFOS and 10:2 FTOH) with the lowest being 4:2 FTOH and fluoride. For the Wcoated graphite tube (Fig 3c), the intensity of fluoride was higher than the other analytes but 4:2 FTOH gave the lowest analytical response. PFOS, PFOA and PFHxS behaved similarly, indicating that the perfluorocarboxylic acids (PFCAs) may have a similar mechanism of interaction with this modifier. They might bind with the carboxylic group rather than the fluorine present in these molecules. Despite the disparate thermal behaviours, when the temperature of the vaporization step was set at 1900 °C, it was possible to obtain similar intensity for all compounds. However, it

was not possible to associate the higher intensity with the same analytical response for all compounds. In such cases, a compromise condition was selected as the optimal conditions for non-specific analysis of fluorine in order to obtain the most similar sensitivity among all PFASs and fluoride. Unfortunately, the low analytical response obtained for 4:2 FTOH and 8:2 FTOH in comparison to the other analytes (even with an optimised temperature program) could not be resolved. This is most likely due to the very volatile nature of these compounds. Thus, these two compounds were excluded from further studies and the method considered unsuitable for short-chain FTOHs and most likely to other neutral and volatile PFASs. Two distinct conditions were set for further sensitivity studies: 600 °C and 1900 °C for the pyrolysis and vaporization steps, respectively, in a Zr-coated graphite tube, and 700 °C and 1900 °C for the pyrolysis and vaporisation steps respectively in a W-coated graphite tube.

## 3.3 Ca/F molar ratio

The ratio between the forming-reagent and analyte were studied for each substance (PFOA, PFOS, PFHxS, 10:2 FTOH and F). Since there is a possibility of the functional groups compete by the forming-reagent with fluorine (eg. the formation of Ca-S or Ca-H), the concentrations of Ca were studied to avoid loss of sensitivity caused by interference. Mass ratios between 0 – 14000 Ca/F were carried out in a 400 µg W-coated graphite tube and the optimised temperature program was applied. According to this study, it is necessary to have a large excess of forming-reagent to achieve the highest intensity signal. For all analytes, the increase in sensitivity is more pronounced up to a ratio of 4000, with only a slight increment up to 12000, where a plateau is achieved. Since no decrease in intensity is noticed with higher

concentrations and the forming-reagent is not considered hazardous, the ratio of 12000 Ca/F was chosen.



**Figure 4.** Optimisation of Ca/F ratio for (■) fluoride; (△)10:2 FTOH; (▼) PFOA; (□) PFHxS and (★) PFOS performed with 25 ng of F.

## 3.4 Sensitivity and calibration curves

PFAS analysis is normally performed in methanolic media (e.g., as EOF), usually following SPE extraction, due to its compatibility with HPLC in reverse phase mode. However, most of the HR-MAS fluorine analyses were carried out with aqueous standards using an inorganic fluoride salt (most commonly KF and NaF) [23–25] Since the PFASs presented unique physical-chemical properties, the sensitivity of these compounds could differ from each other and vary with the solvent used. Furthermore, the solubility of fluoride cannot be guaranteed in every solvent.

For this reason, a study of the calibration curve slopes was carried out with each of the selected compounds (PFOA, PFOS, PFHxS, 10:2 FTOH and F<sup>-</sup>) in aqueous and methanolic solution. The PFASs PFHxA, PFDA and PFHpA in Zr-coated and W-coated graphite tubes were also studied in order to see whether all PFCA behave similar.

## 3.4.1 Aqueous external calibration

The aqueous calibrations were performed between 1.5 ng - 5 ng (5  $\mu$ L of 0.3 to 1.0 mg L<sup>-1</sup>), using 50  $\mu$ g of Ca as the forming reagent, Zr and W as permanent modifiers in the optimised conditions and compared with a method proposed by Mores et al. [28] which also used external aqueous calibration and no permanent modifier. The slope for each PFASs are shown in Table 5.

**Table 5.** Aqueous calibration curve slopes obtained using W-coated and Zr-coated graphite tubes with the optimised conditions and calibration curve slopes obtained with the method described by Mores et al. [28]. Average and error are given as standard deviation of triplicates.

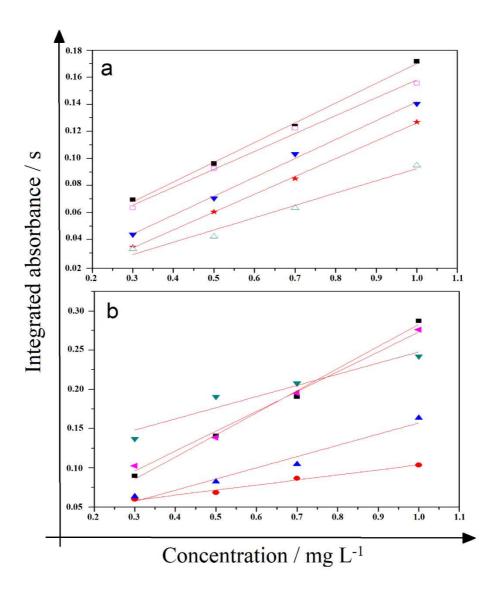
W-coating		Zr-coatir	Zr-coating		Mores method	
Compound	Slope	R	Slope	R	Slope	R
	(mg L <sup>-1</sup> )		(mg L <sup>-1</sup> )		(mg L <sup>-1</sup> )	
F	0.121 ± 0.03	0.998	0.164 ± 0.01	0.996	0.251 ± 0.01	0.997
PFOA	$0.116 \pm 0.01$	0.989	$0.104 \pm 0.01$	0.988	0.115 ± 0.01	0.964
PFOS	$0.124 \pm 0.01$	0.987	0.136 ±0. 01	0.991	$0.194 \pm 0.03$	0.969
PFHxS	0.112 ± 0.01	0.992	$0.088 \pm 0.01$	0.998	$0.199 \pm 0.03$	0.992
10:2 FTOH	0.062 ±0.01	0.987	0.086 ± 0.01	0.963	0.079 ± 0.01	0.992

A Tukey-Kramer test was applied to evaluate the variance between the three studied methods: Using the optimized conditions presented in this work (for Zr as permanent modifier and W as permanent modifier) and without permanent modifier (according to Mores et al.[28]) and suggested that for a 95% confidence level), the methods did not show a significant difference. However, there is too much noise in the studied data. In this case, an individual analysis of each set of data was needed to evaluate the randomness of the data.

When W was used as permanent modifier (Fig. 5-a), a lower variation between the PFASs slopes was achieved when compared with the inorganic aqueous standard. The lowest variation was achieved for PFOS, which was 2% lower compared to fluoride using a W-coated tube, while the higher difference was presented by 10:2 FTOH– 51% when compared with the inorganic fluoride slope. According to a 2-tailed 95% confidence t-test, excepted by 10:2 FTOH, the slopes did not present any significant difference. This means that a calibration with fluoride would be useful for the ionic PFASs with low volatility.

The results obtained with the W-coated graphite tube and the optimised conditions can be compared with the method established by Mores et al. [20] for the same analytes (Fig. 5-b). The sensitivities of the different PFASs obtained by this method, using a graphite tube without permanent modifier, pyrolysis temperature of 725 °C and vaporisation temperature of 2250 °C were completely different. The comparison of the averages varied between 20% for PFHxS and 68% for 10:2 FTOH when the slopes are compared to the average of F<sup>-</sup> calibration curve. According to a 95% confidence 2-tailed t-test, only PFHxS slope was statistically similar with fluoride slope. The method described by Mores et al. [20] seems unsuitable for the determination of extractable organofluorines, being more appropriated the use of W

in the optimised conditions, due to the lower difference of sensitivity between the studied compounds.



**Figure 5**. Aqueous standard calibration curve for fluorine from (■) fluoride; (●) 10:2 FTOH; (▼) PFOA; (★) PFHxS and (▲) PFOS in a) 400 μg W-coated graphite furnace and optimized conditions (T<sub>pyr</sub>: 700 °C/ T<sub>vap</sub>: 1900 °C)(this study) and b) without permanent modifier, according to Mores *et al.* [28] (T<sub>pyr</sub>: 725 °C/ T<sub>vap</sub>: 2250 °C).

Since the present method was developed to be a tool for mass balance for EOF (extractable organic fluorine), the study of sensitivity was evaluated using methanolic calibration curves, once the methanolic solutions presented a slightly different sensitivity when compared to the aqueous solution. This experiment was performed in the same calibration range, between 1.5 ng – 5 ng F (5  $\mu$ L of 0.3 to 1.0 mg L<sup>-1</sup>), using 50  $\mu$ g of Ca as the forming reagent, and Zr and W as permanent modifiers with the optimised temperature conditions. The 10:2 FTOH was not studied in methanolic media because it is not extracted with the chosen sample preparation method. The slopes for both permanent modifiers are shown in Table 6. Since the method described by Mores *et al.* (20) was applied only for aqueous standards and samples, it was not used as comparison for this study.

**Table 6.** Methanolic calibration curve slopes obtained with W-coated and Zr-coated graphite tube with the optimised conditions to determine total F in EOF. Average and error are given as standard deviation of triplicates

	W-coating		Zr-coating		
Compound	slope (mg L <sup>-1</sup> )	R	slope (mg L <sup>-1</sup> )	R	
F	$0.159 \pm 0.02$	0.988	$0.263 \pm 0.02$	0.996	
PFOA	$0.092 \pm 0.06$	0.999	$0.127 \pm 0.02$	0.986	
PFOS	$0.099 \pm 0.01$	0.961	$0.106 \pm 0.06$	0.996	
PFHxS	$0.101 \pm 0.01$	0.962	$0.128 \pm 0.01$	0.957	
PFHxA	$0.098 \pm 0.03$	0.982	$0.125 \pm 0.01$	0.994	
PFHpA	$0.098 \pm 0.03$	0.982	$0.085 \pm 0.01$	0.991	
PFDA	$0.092 \pm 0.03$	0.969	0.111 ± 0.02	0.989	

It is obvious that using a methanolic solution fluoride cannot be used as calibrant for the different PFAS both coatings, due to the discrepant sensitivity when compared to the other species. For the calibration performed in a Zr-coated graphite tube, the PFASs slopes presented a relative difference from 52% to 68 % – when compared with the aqueous F<sup>-</sup> standard. However, the sample preparation aims to the µµdetermination of total fluorine in the extractable organofluorines (EOF), and the concentration of F<sup>-</sup> is negligible since it would not be extractable in the non-polar solvents. Comparing the averages of the slopes of all compounds with the PFOA calibration curve, the variation of the slopes was between 1% for PFHxS and 32% for PFHpA. The other standards gave slopes between 2% and 17%. According to a 95% confidence 2-tailed t-test, with exception of PFHpA, no significant differences were found between PFOA and the other PFASs.

For the W-coated graphite tube, the slope variation of the PFASs when compared with F<sup>-</sup> was also high, from 36% to 50%. However, when the slopes are compared with the PFOA calibration curve, the difference among them was lower than 15%. 2-tailed t-tests with 95% confidence between PFOA slope compared with the other PFASs were evaluated, and no significant difference were found for any of the studied compounds. For this reason, W-coated graphite tube was chosen for the quantification of total fluorine of the EOF.

3.5 Figures of merit and the determination of total organic-F in river, seawater, wastewater and effluent samples using SPE sample preparation

A brand new graphite tube was coated with 400 µg W to provide a higher sensitivity and lower standard deviation, since a poorly coated or porous surface can

affect negatively the obtained results. The temperature program was set according to the optimised conditions (Table 1). The calibration curve was constructed using PFOA standard solutions with subsequent use of SPE according to the session 1.3 of this present work, in a working range of 1.5 ng – 7.5 ng F. The sample volume was fixed to 5  $\mu$ L of sample to avoid deviations caused by an incomplete dry of higher volumes. It was used 12  $\mu$ L of a 1% Ca solution as forming reagent. The samples were enriched with a mix of PFOA, PFOS, PFHxS, PFHxA, PFHpA and PFDA. In order to fit in the working range, the samples were diluted in methanol around 100 times just before the analysis and the final concentration were 5  $\mu$ g L<sup>-1</sup> and 10  $\mu$ g L<sup>-1</sup>. The limit of detection and quantification were calculated based on 3 and 10 times the standard deviation of 10 measurements of blank divided by the calibration curve slope, respectively. The limit of detection for the method using SPE as sample preparation was 0.3  $\mu$ g L<sup>-1</sup> and the limit of quantification was 1  $\mu$ g L<sup>-1</sup>. A summary of the figures of merit is shown in Table 7.

**Table 7**. Figures of merit for fluorine determination *via* CaF under optimised conditions and SPE methanolic PFOA extract standard external calibration.

Parameter	Value
Equation	y= 0.159x + 0.031
$R^2$	0.999
LOD inst	0.1 mg L <sup>-1</sup>
LOQ inst	0.3 mg L <sup>-1</sup>
LOD <sub>SPE</sub>	0.3 μg L <sup>-1</sup>
LOQ <sub>SPE</sub>	1.0 μg L <sup>-1</sup>
Working range	0.3 mg L <sup>-1</sup> - 1.5 mg L <sup>-1</sup>

The recovery rate for the selected samples (Table 8) was satisfactory, especially when considering the complexity of the matrices. The wastewater samples had the lowest recovery rate (around 72%). However, this complex matrix presented a high level of dissolved solids. It is well known that PFASs are easily adsorbed [40], which could explain the low recovery rate, since only the fluorine present in the supernatant is quantified.

**Table 8**. Concentrations and recovery of total F from PFASs enrichment (spike), after extraction by SPE (n=3).

		Percent recovery		
Sample	unspiked matrix (µg F L <sup>-1</sup> )	5 μg F L <sup>-1</sup>	10 μg F L <sup>-1</sup>	
Sea water	<1.0	103 ± 17%	80 ± 2%	
River water	14.5 ± 0.1	112 ± 3%	101 ± 3%	
Effluent	<1.0	136 ± 9%	85 ± 1%	
Wastewater	<1.0	68 ± 2%	75 ± 2%	

## 4. Conclusion

The present paper showed that different organofluorine compounds exhibit different thermal behaviour and sensitivity for HR-GF MAS for total F quantification via CaF. Through an optimisation of temperatures and permanent modifiers, it was possible to achieve similar sensitivities among selected PFASs with different perfluoroalkyl chain lengths and functional groups. However, the developed method proved to be unsuitable for short chain FTOHs, which had extremely low sensitivity when compared to the other PFASs due its high volatility and loss in the drying step. This work introduces a completely new approach to total fluorine determination,

since most papers only work with inorganic standards and aqueous media, which is
not applicable for the mass balance of organofluorine. The combination of a sample
preparation method to preconcentrate the analyte and the optimised temperature
program allowed low limits of detection and quantification to be achieved, making it
possible to quantify total F in the low ppb range. Although other possible
organofluorines such as F-containing pharmaceuticals require further testing, this is
a first approach to optimise the modifiers and temperature programmes for PFAS
determination in complex environmental samples. The developed method can
therefore be used for total fluorine determination in organic extracts or in the often
used EOF (extractable organofluorines) when only ionic PFASs such as PFCAs and
PFOS occur.

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## Highlights:

- Response optimisation for individual PFAS
- Same response for ionic extractable organofluorines using HR-GF-MAS
- Low response for volatile neutral PFAS
- Validation for total fluorine determination of PFCAs in water samples

Declaration of interests
oxtimes The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.
☐The authors declare the following financial interests/personal relationships which may be considered as potential competing interests: